

SPE165433

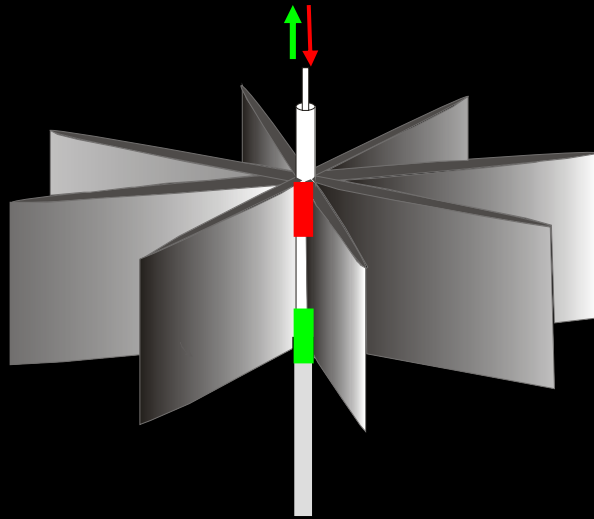
Vertical Single-Well SAGD with Multiple Producers

Grant Hocking¹ and Dale Walters²

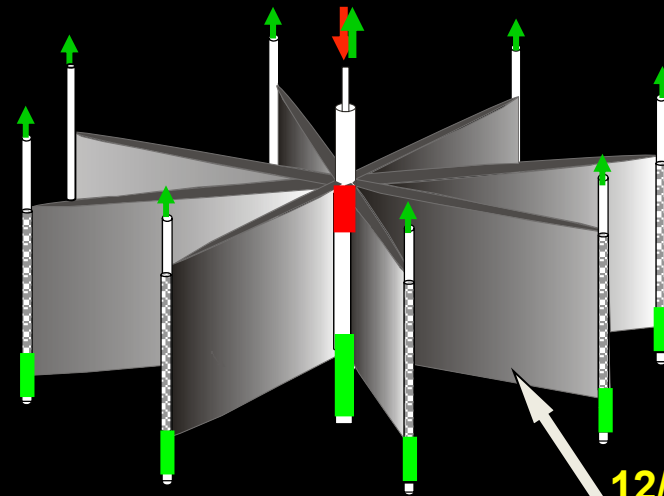
¹GeoSierra, ²Taurus Reservoir Solutions

Frac Enhanced SAGD

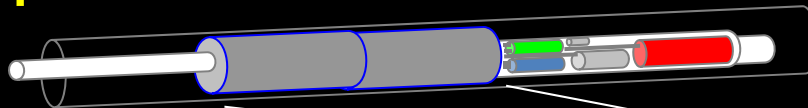
Single-Well SAGD



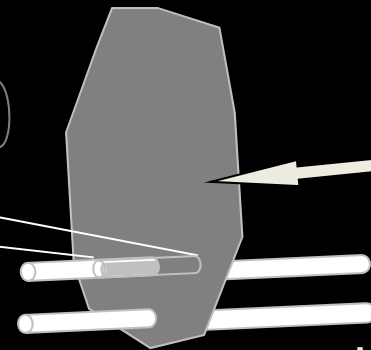
Single-Well SAGD with Multiple Producers



Hz open-hole stimulation



12/20 Garnet



Unconsolidated Formations

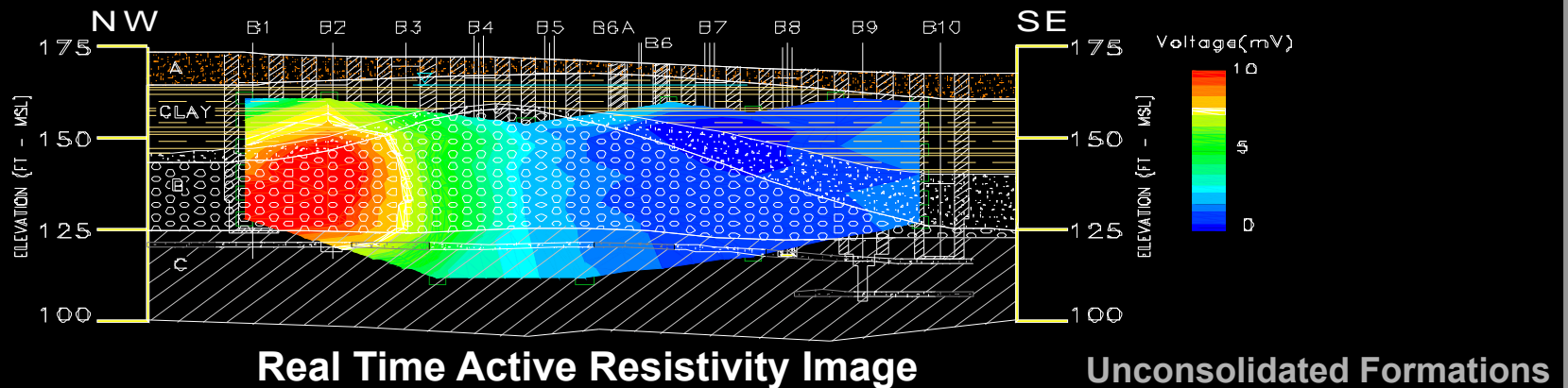
Azimuth Controlled Fracturing

Slide 3



Azimuth Controlled Fracturing

Slide 4

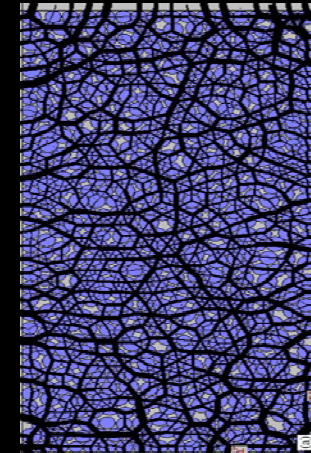


Non-Brittle Weak Formations

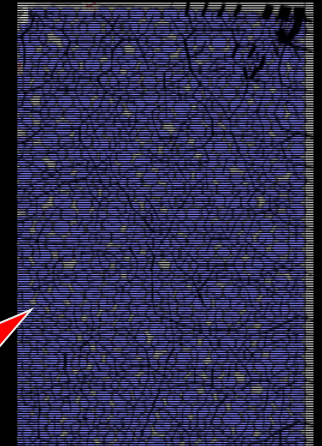
Weakly Cemented Formations

- Minimal Cementation, Soft & Weak
- Stress State
 - **Force Chains Fragile**
 - Easily Destroyed
 - Minor Vibration or Shearing
 - Grain Contact Dissolution
 - Over-Pressurization
 - **Minimal Horizontal Stress Contrast**
 - Horizontal Stress Contrast can not be maintained over geological time
- Constitutive Behavior
 - **Ductile Frictional Behavior**
 - **Anelastic**
 - **Skempton's B parameter**

Isotropic Compression Force Chains Shown



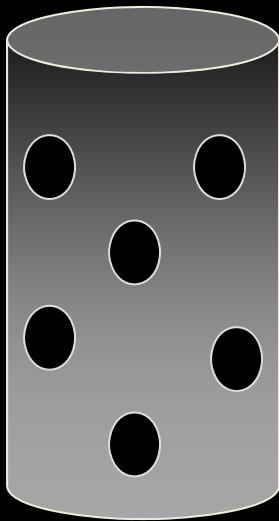
Force Chains Destroyed



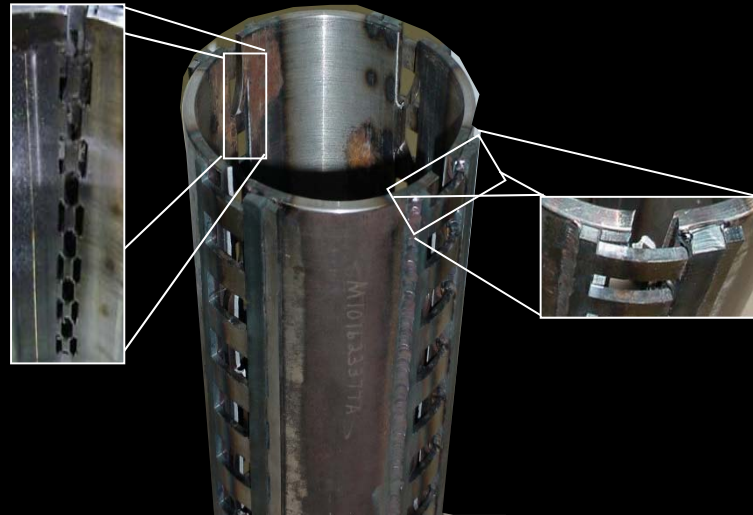
Minor Shear Strain
Destroys Force Chains

Offset Well Stimulation Comparison

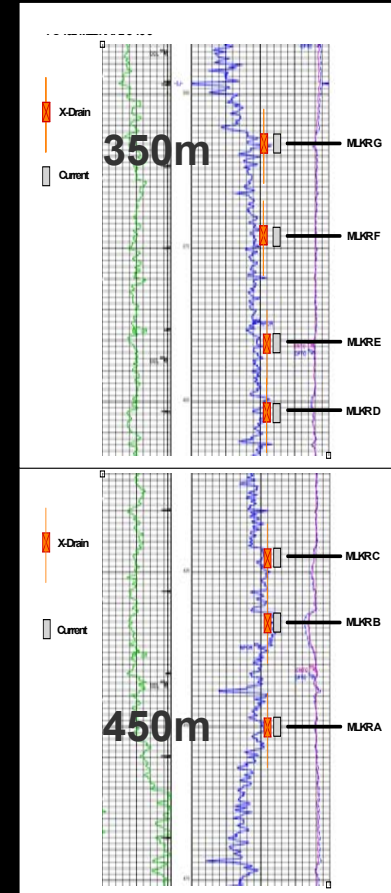
Perforations



Dilating Casing



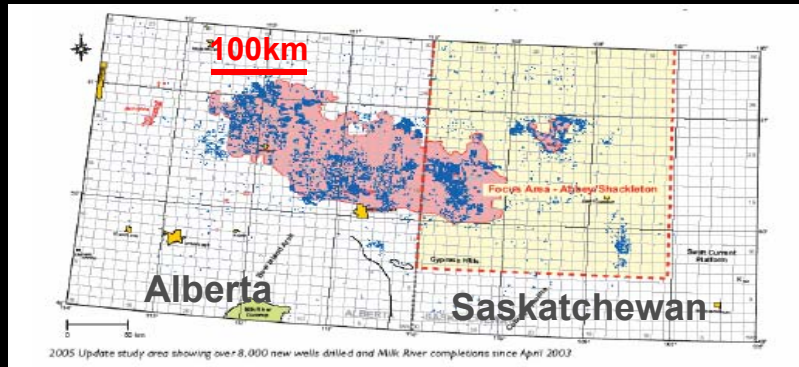
Milk River



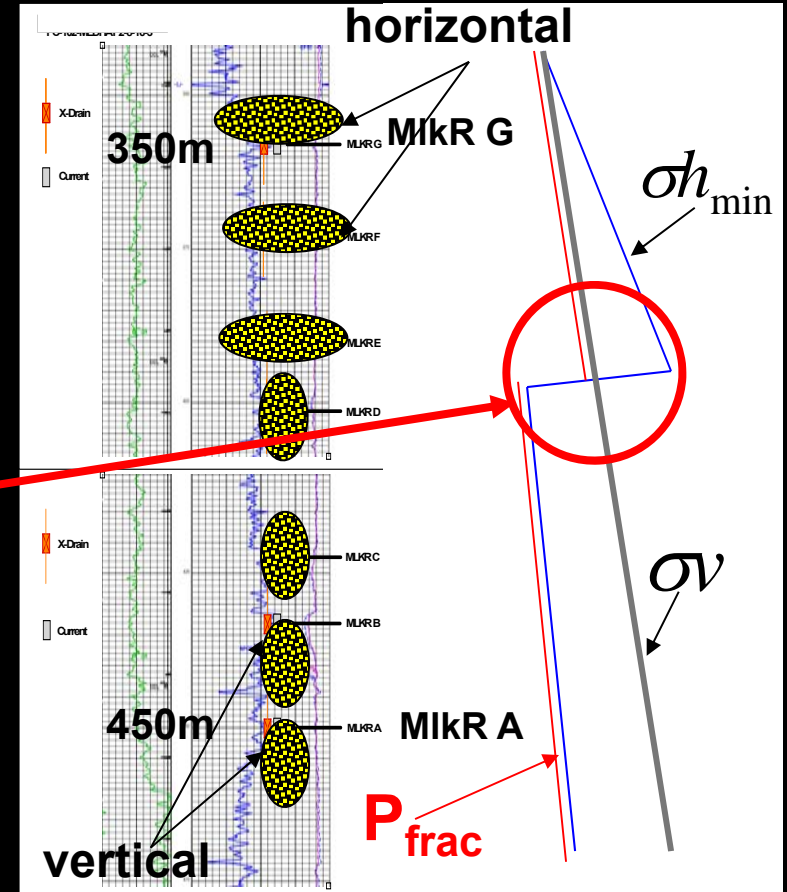
Milk River Tight Gas Reservoir

Non-Brittle Weak Formation

- $E \sim 3\text{GPa}$ $c' \sim 2.5\text{MPa}$ $\phi \sim 35^\circ$ $UCS^* \sim 10\text{MPa}$
- 40,000 wells conventionally stimulated
- CO_2 fluid 20/40 sand 10tons/horizon
- Surface & Downhole Tiltmeter Arrays
- Injection Pressures $\uparrow \sim 40\%$ at $< 400\text{m}$ depth
- Vertical 'Frac' $> 400\text{m}$ Horiz 'Frac' $< 400\text{m}$
- **Stress Crossover at 400m**



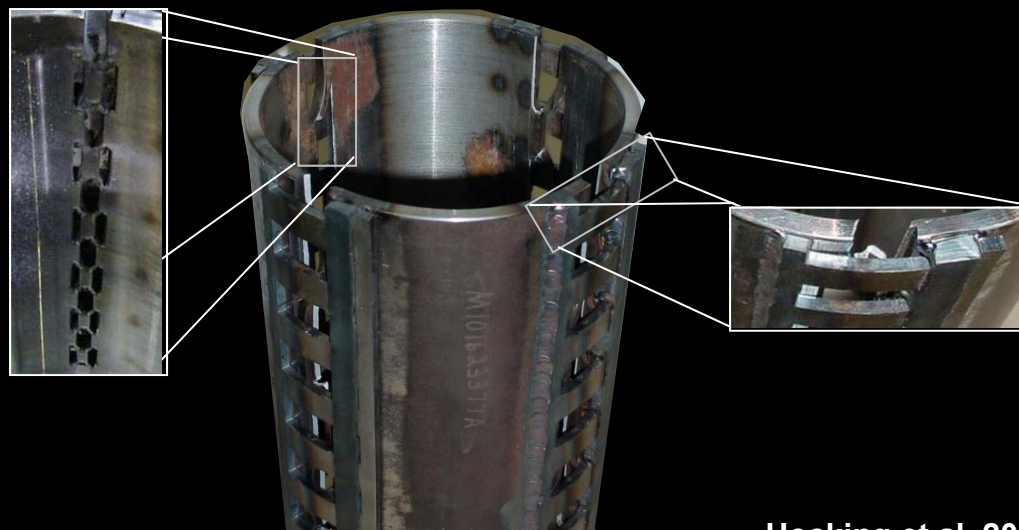
Note: $UCS^* = 2c' \tan(45 + \phi/2)$



Milk River Tight Gas Reservoir

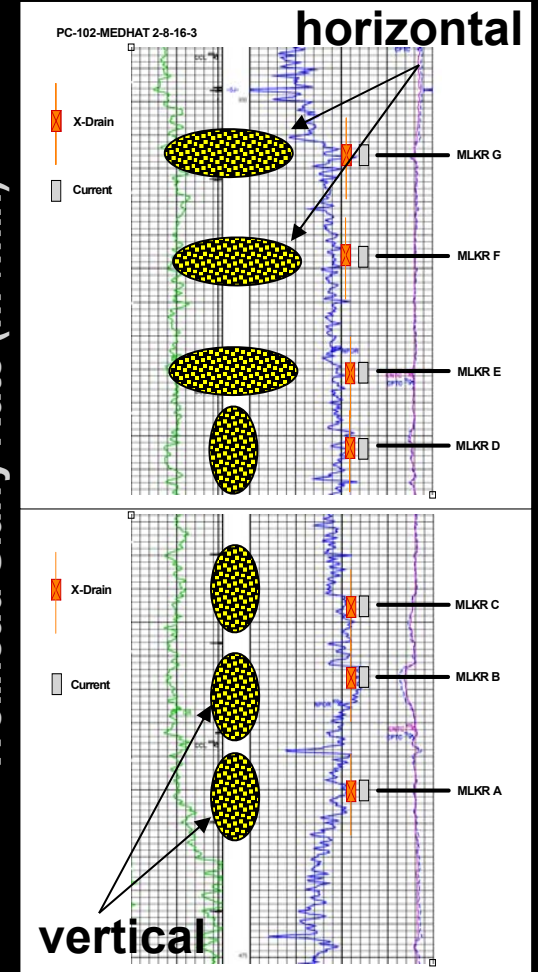
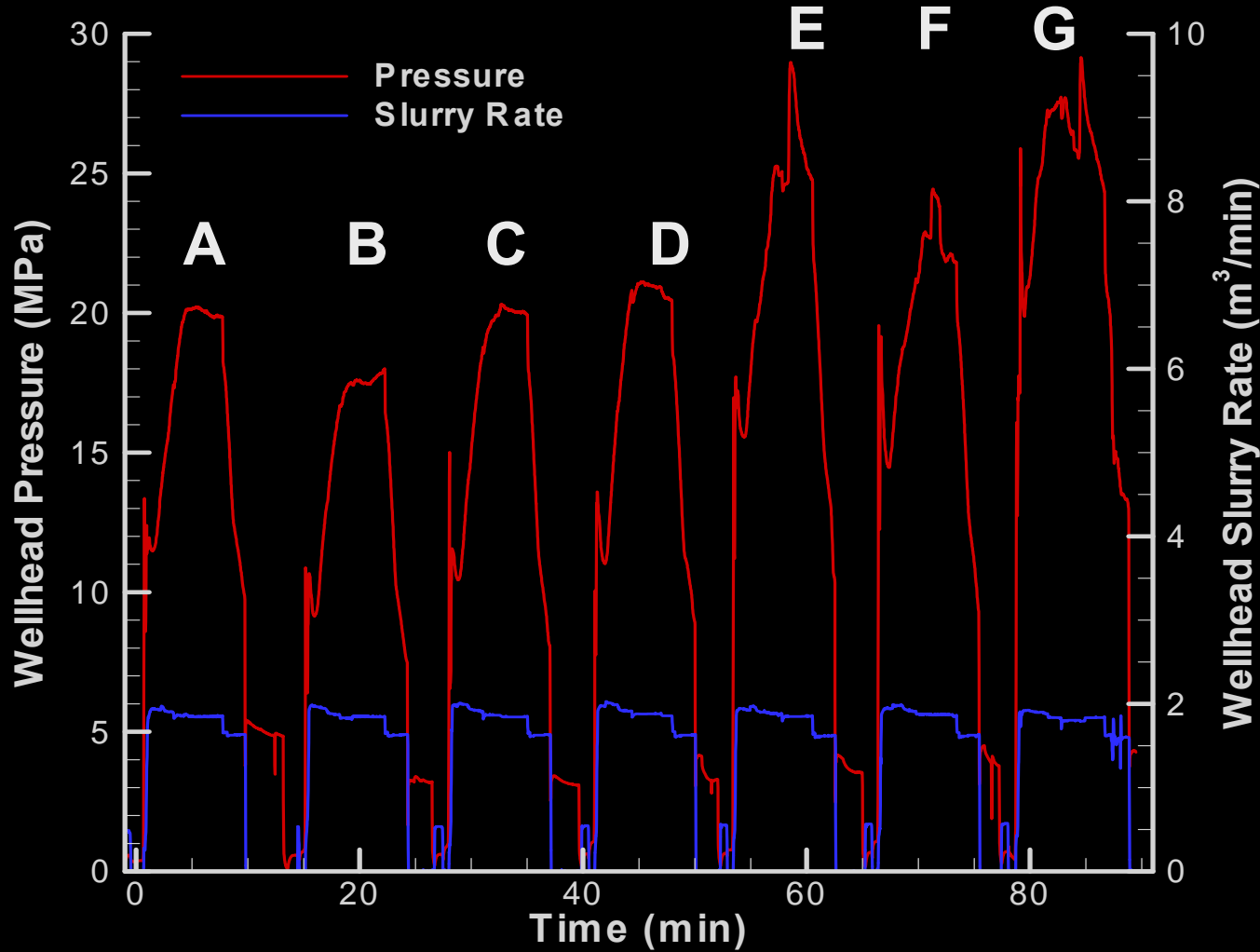
Stimulation Split Dilating Casing

- Cemented by Inner String
- Mechanically Split & Expanded
- 10% Radial Strain
- Locked in Open Position
- Multiple Wings intersect Formation
Shoreline Anisotropy



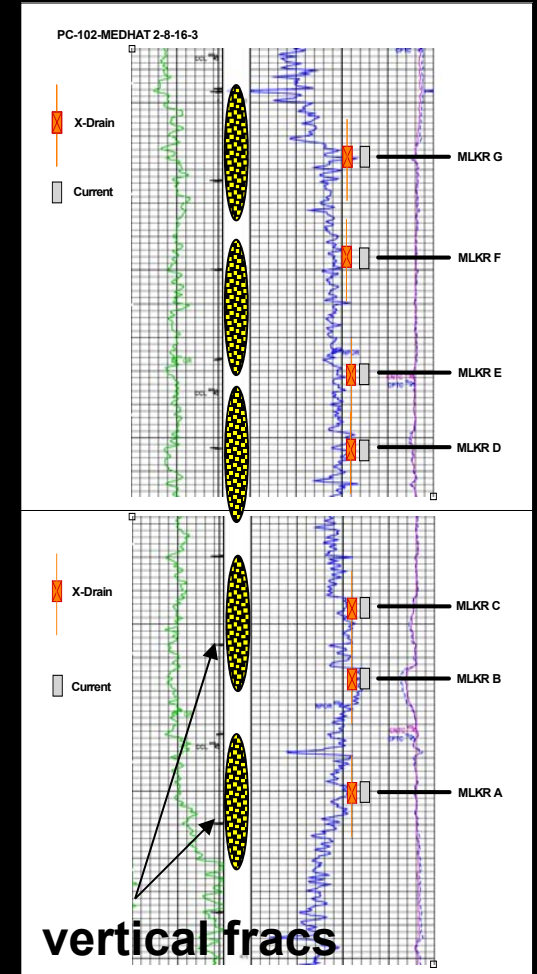
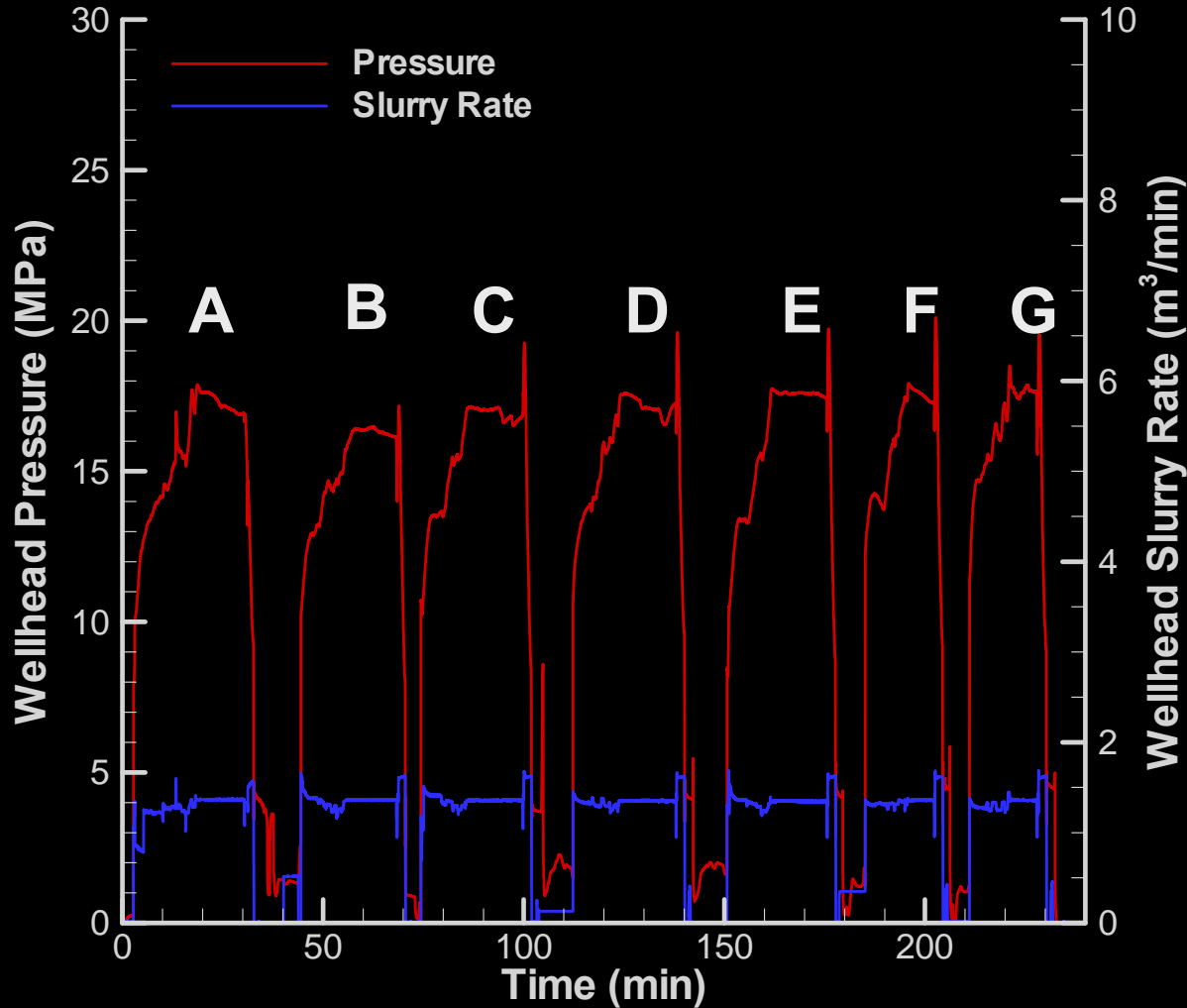
Hocking et al. 2011

Conventional Stimulations



Hocking et al. 2013

Split Dilating Casing Stimulations

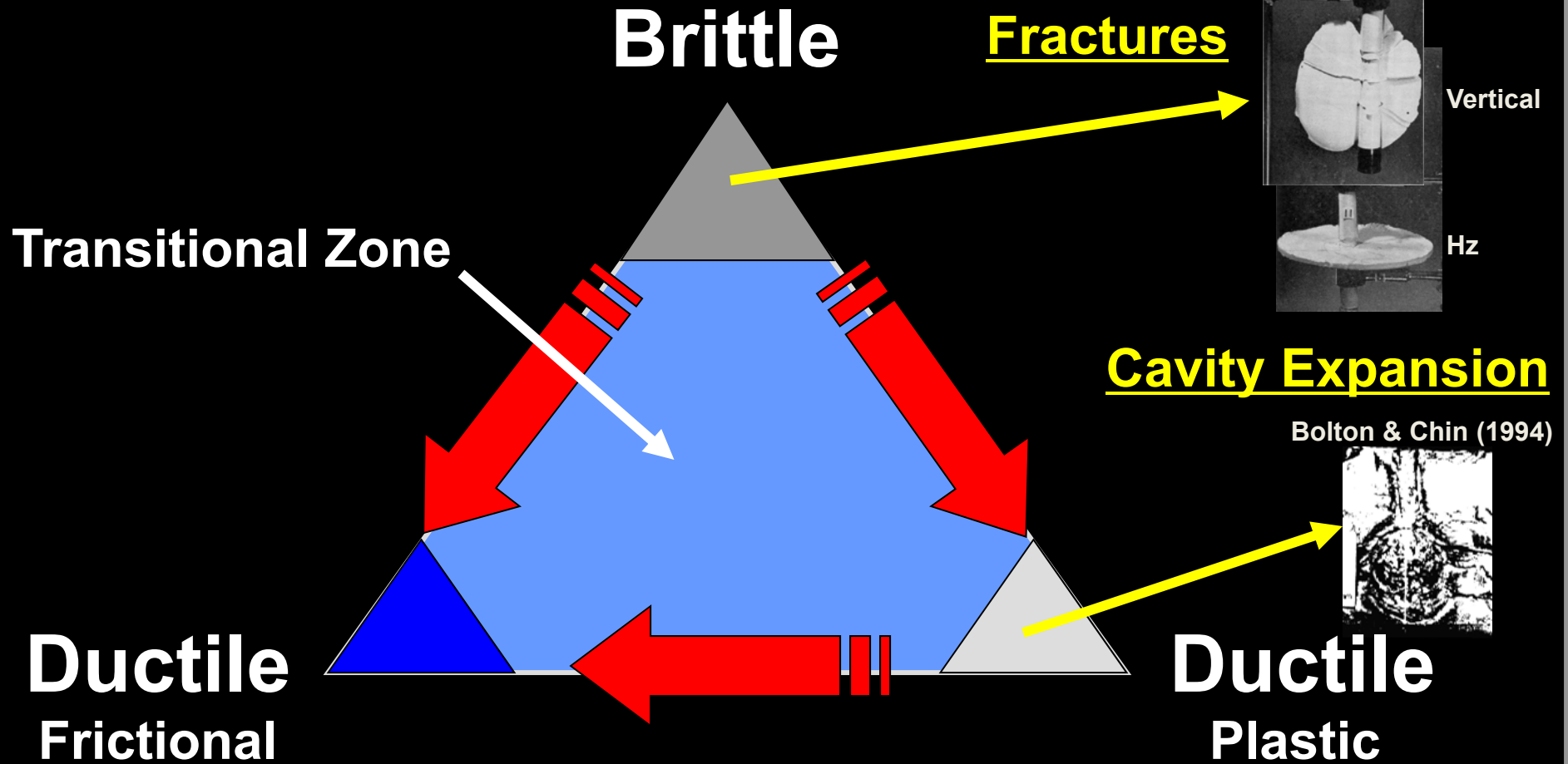


Hocking et al. 2013

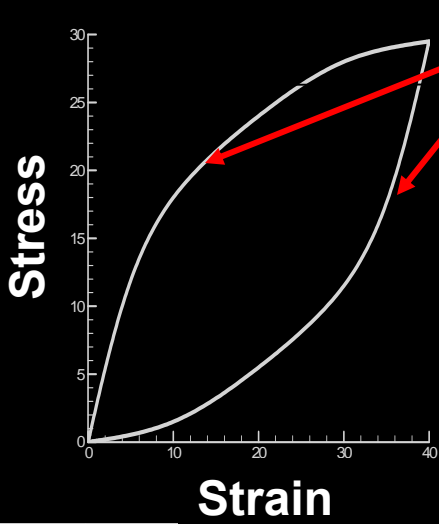
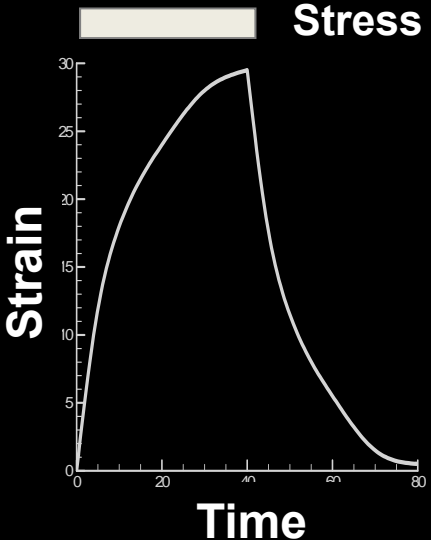
Lessons Learnt

- **Completion Method Controls the Outcome**
 - How do you interpret stimulation and shut-in pressure records?
 - Mapping injected geometries only tells you of the outcome
 - Stimulation thru' perfs or open-hole do not excite least energy dissipating mechanism
 - Frac initiation is essential
- **Why? Non-Brittle Weak Formations**
 - Anelasticity
 - Skempton's B Parameter

Brittle Ductile States

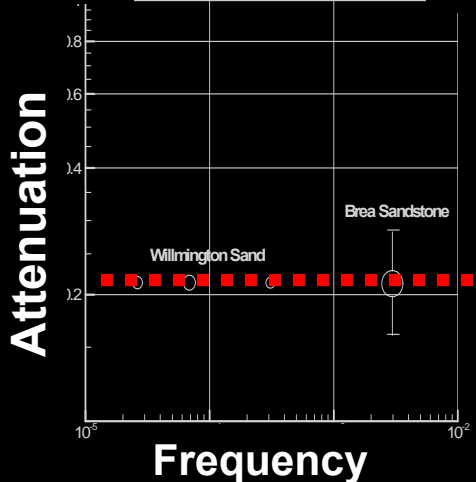


Anelasticity



Loss Factor $\eta = \frac{E''}{E'} = \tan\phi$

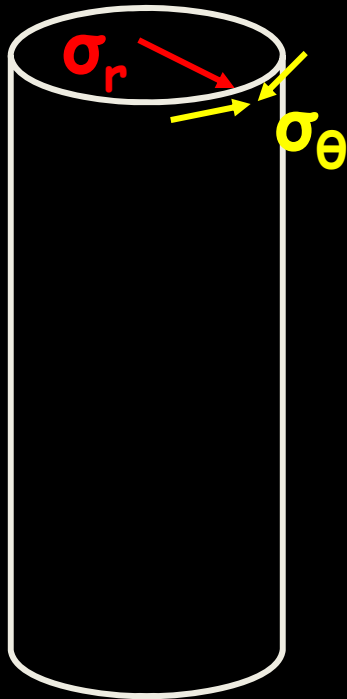
$\eta = \phi = \tan\phi = \frac{\delta}{\pi} = \frac{\psi}{2\pi} = Q^{-1}$



Dry Sand/Weak Sandstone
Q=5 Quality Factor

Anelasticity - Cylindrical Cavity

Field Stress p_0
compression +ve



Linear Elastic

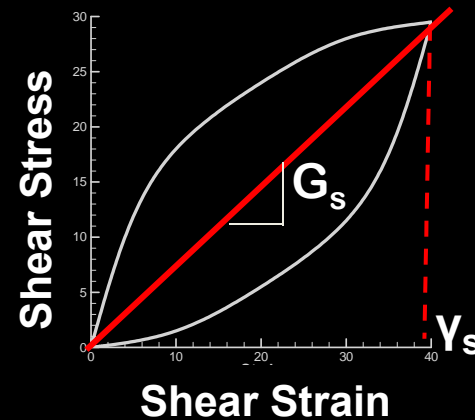
$$\sigma_r = p_0 + \Delta p$$

$$\sigma_\theta = p_0 - \Delta p$$

Non-Linear Elastic

$$\sigma_r = p_0 + \frac{\alpha}{\beta} \gamma^\beta$$

$$\sigma_\theta = p_0 - \alpha \left(2 - \frac{1}{\beta} \right) \gamma^\beta$$



$$\tau = \alpha \gamma^\beta$$

$$\alpha = G_s \gamma_s^{1-\beta}$$

Bolton & Whittle (1999)

$\beta=0.5$	$Q=3$	$\eta=0.3$
$\beta=0.65$	$Q=5$	$\eta=0.2$
$\beta=0.8$	$Q=10$	$\eta=0.1$

Inclusion Tip and Mobility

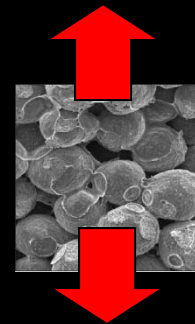
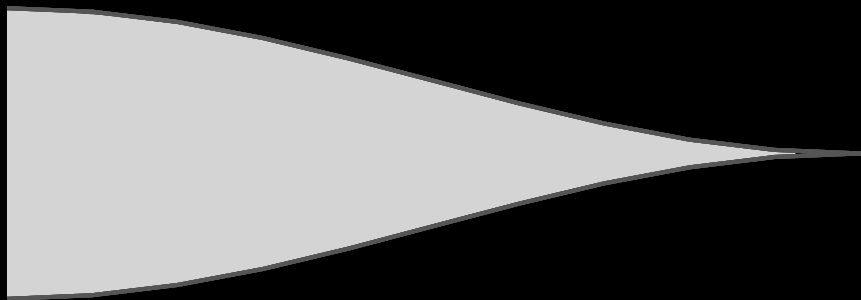
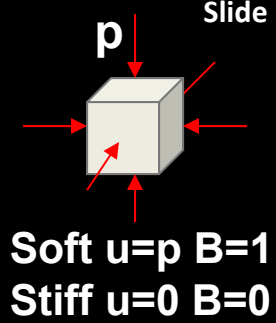


Skempton's B parameter

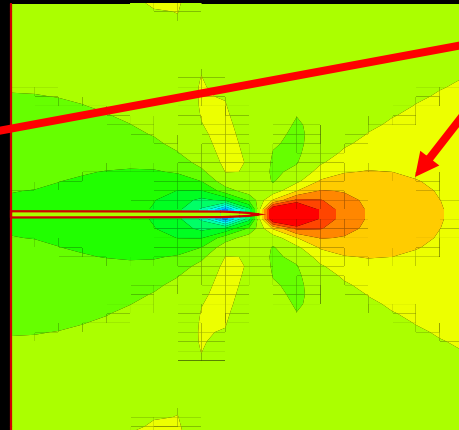
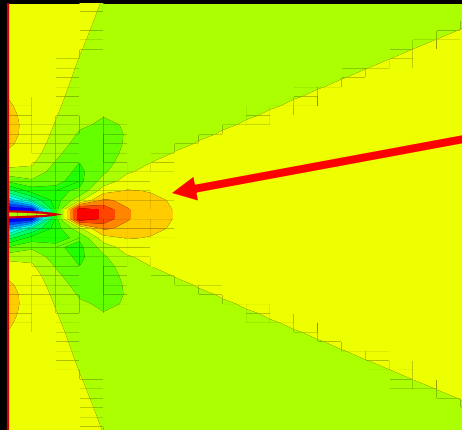
- >0.75 at low p'
- >0.5 at high p' at significant depth

Inclusion Tip Mobility & Geometry

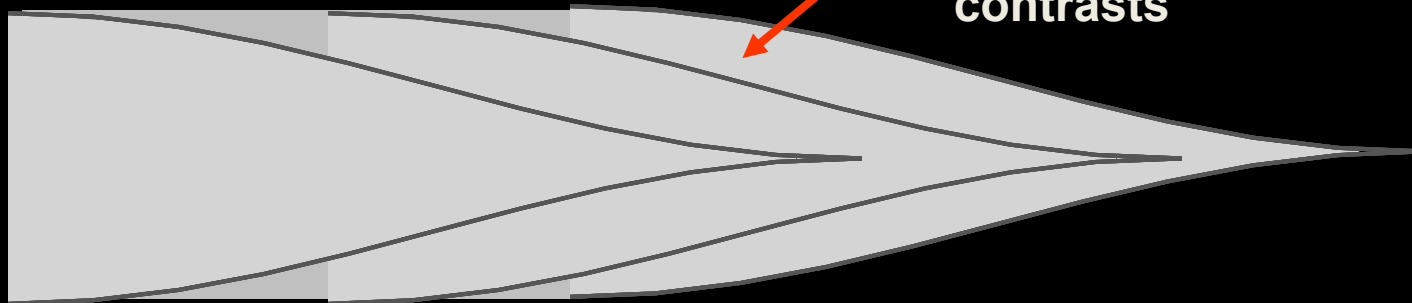
- negative pore pressure in front of tip
- inclusion clamped by apparent cohesion
- inclusion sucked into the unloaded zone
- remains on azimuth due to anelasticity



Inclusion on Azimuth - Anelasticity



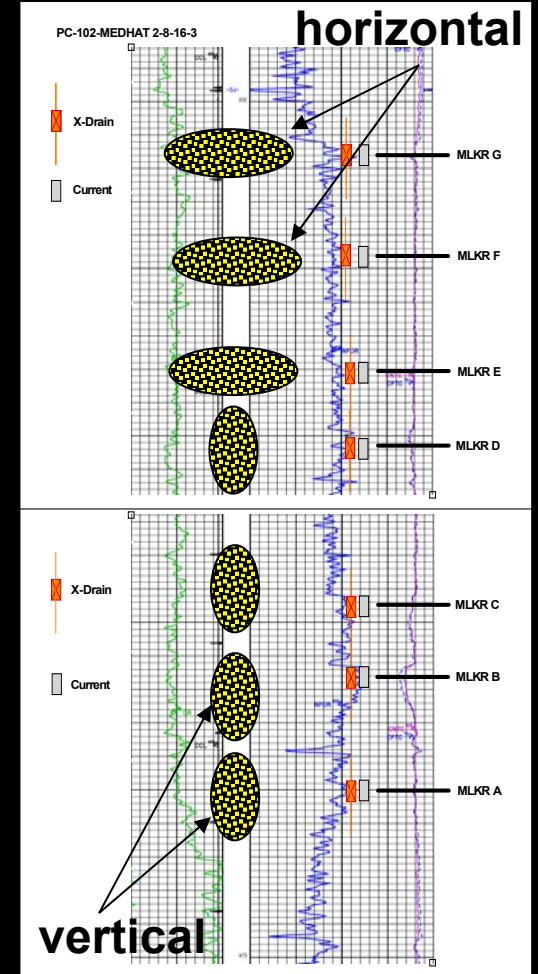
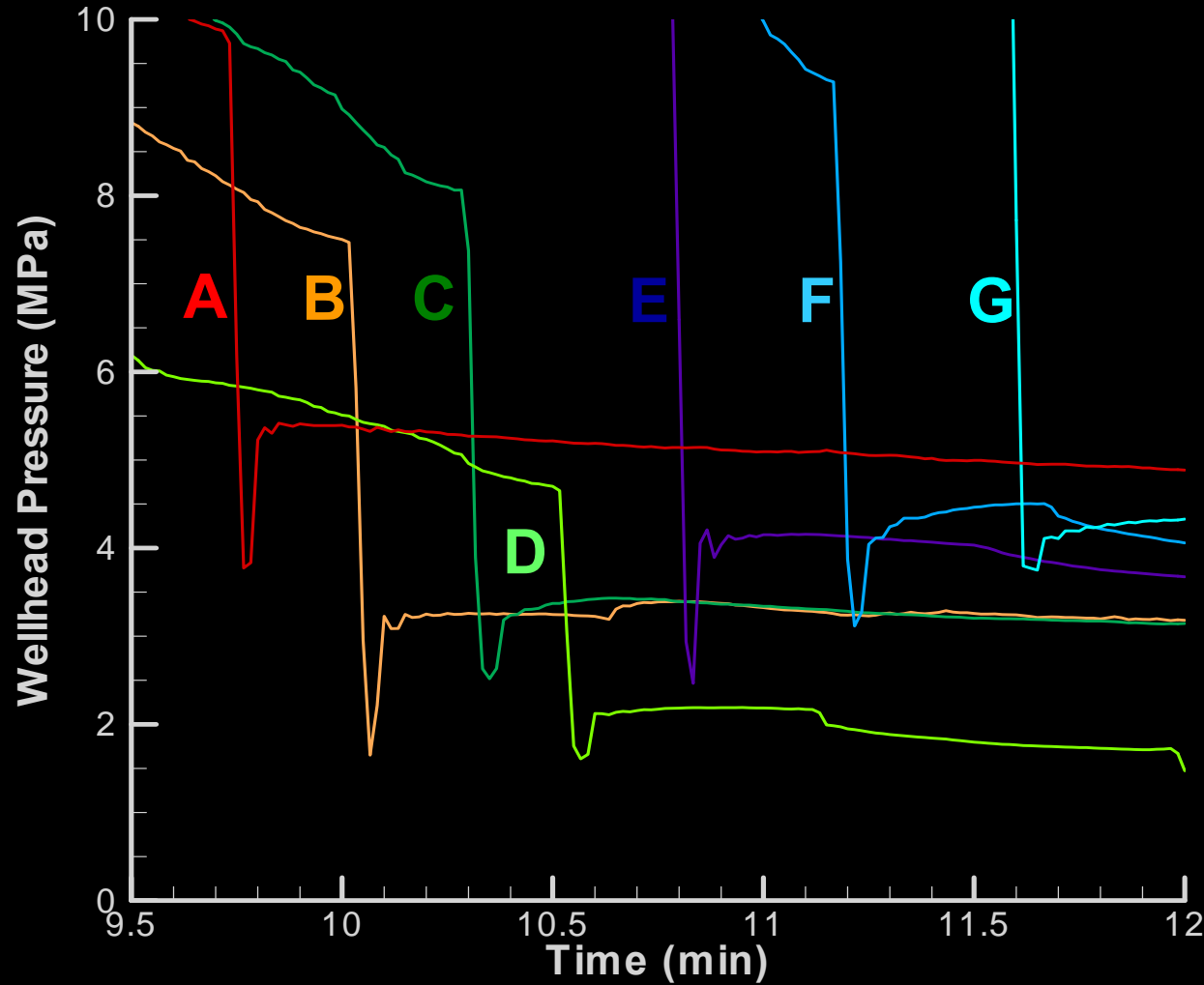
Process zone grows with inclusion length due to anelasticity resulting in a more robust propagating inclusion remaining on azimuth



Propagating inclusion remains on azimuth even with modest stress contrasts

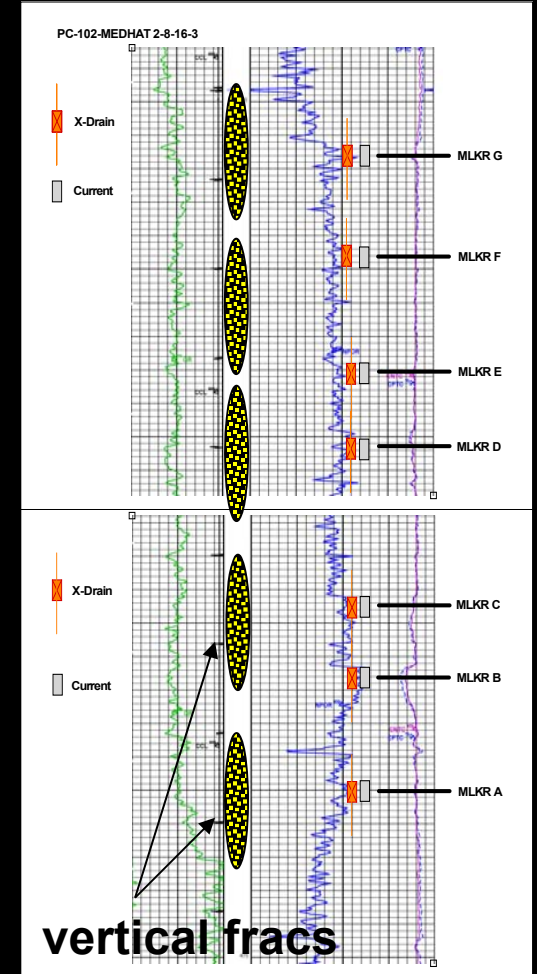
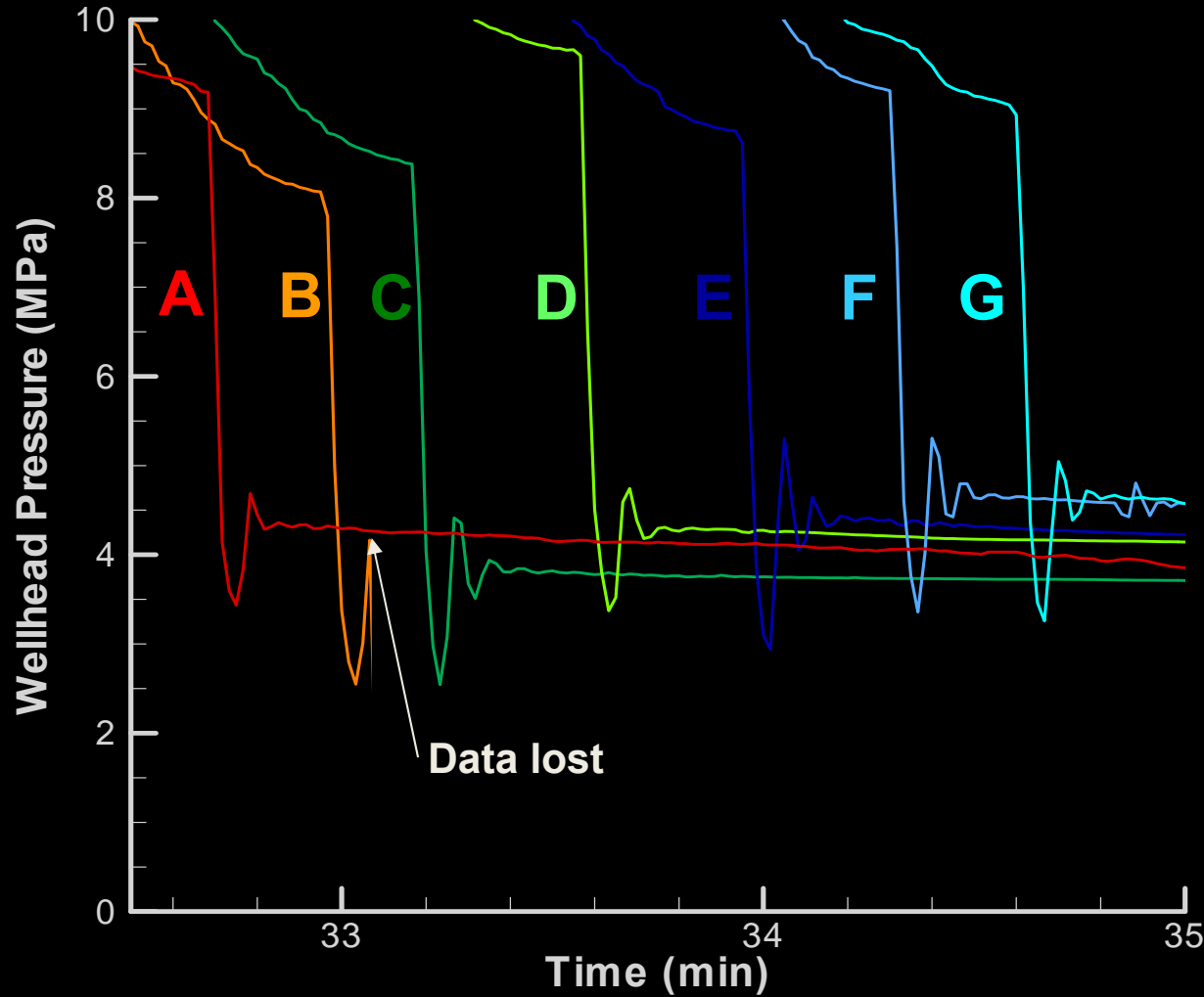
Anelasticity, Skempton's B parameter – no mention of plasticity

Conventional Stimulations



Hocking et al. 2013

Split Dilating Casing Stimulations



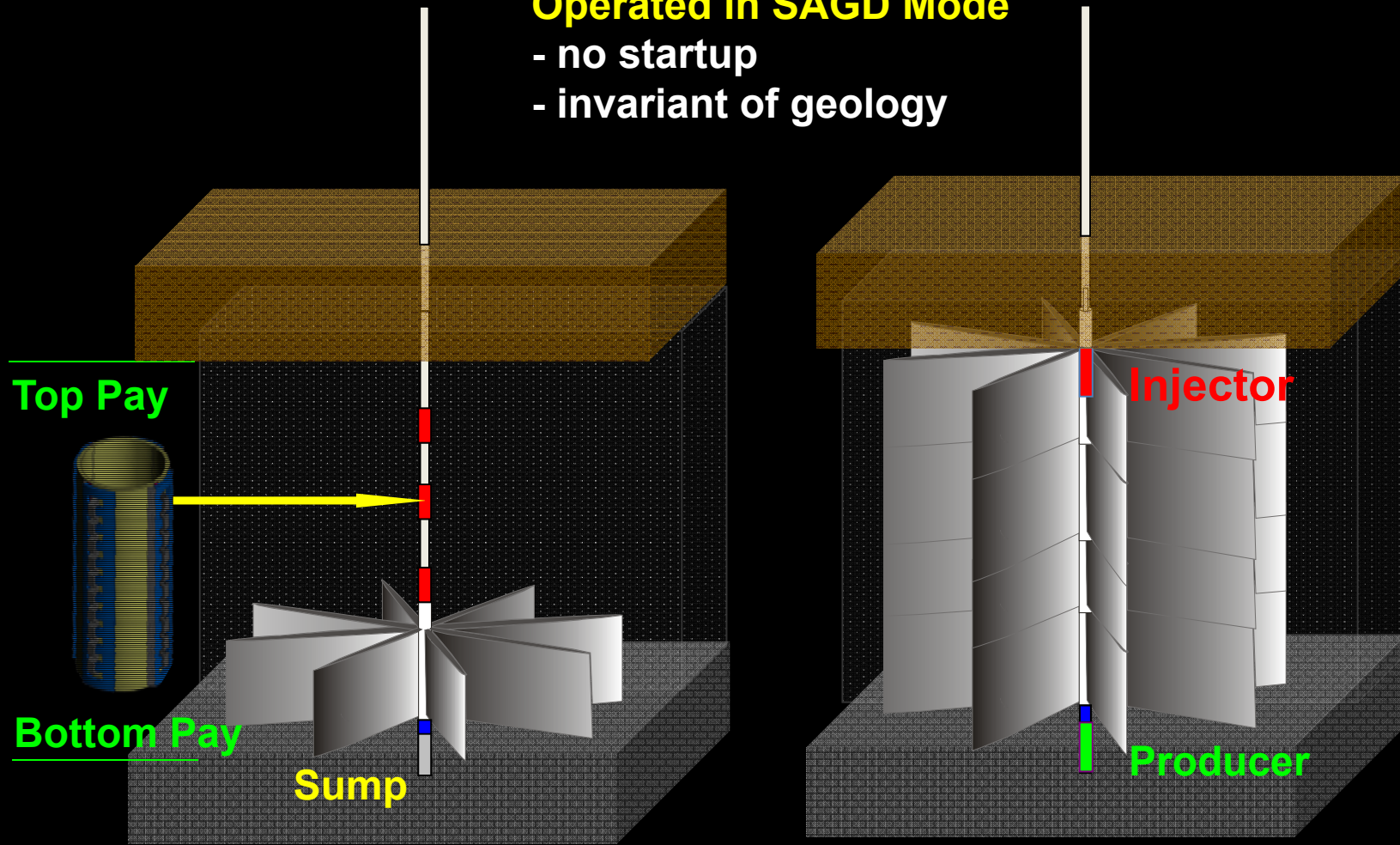
vertical fracs

Hocking et al. 2013

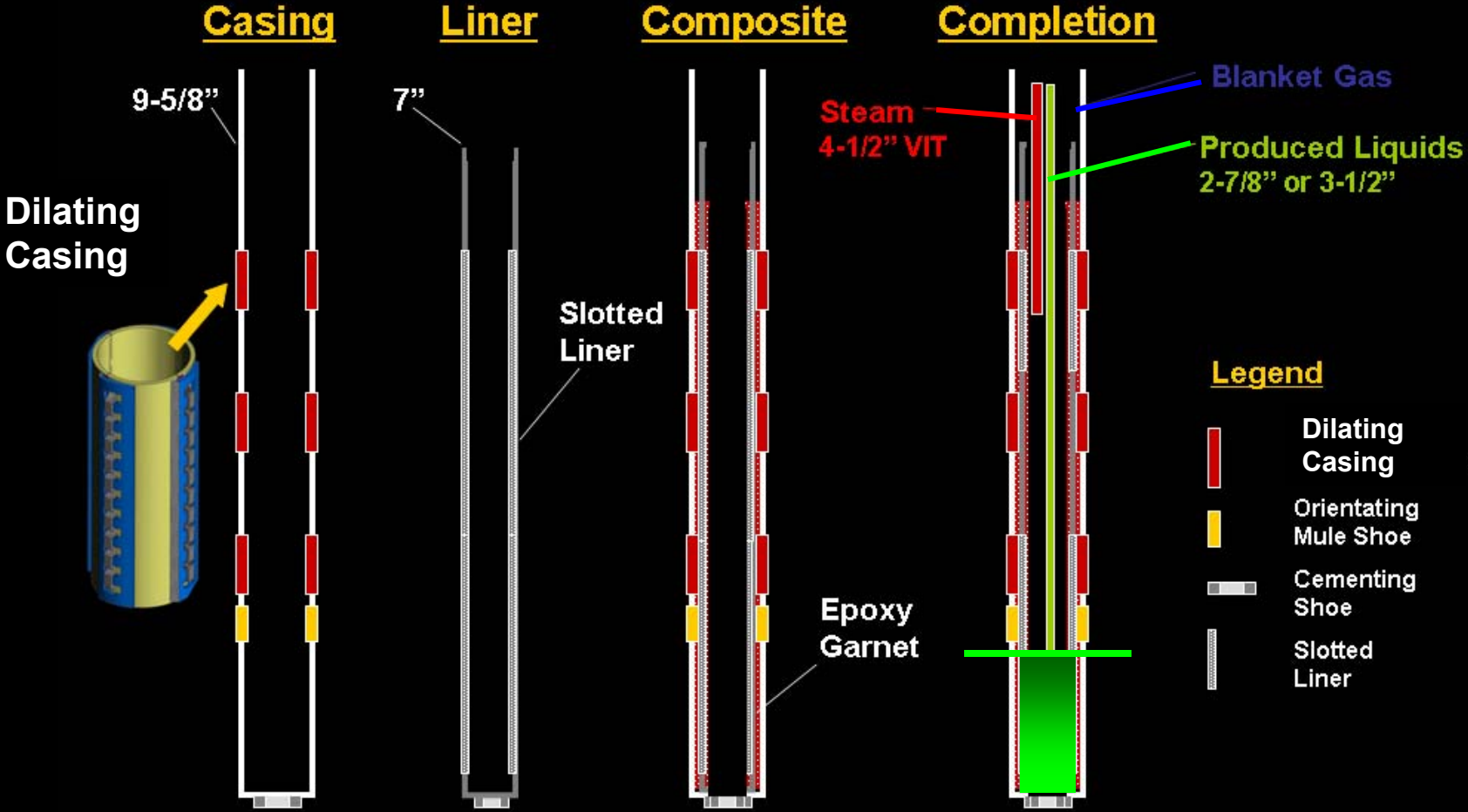
Well Construction Sequence

Operated in SAGD Mode

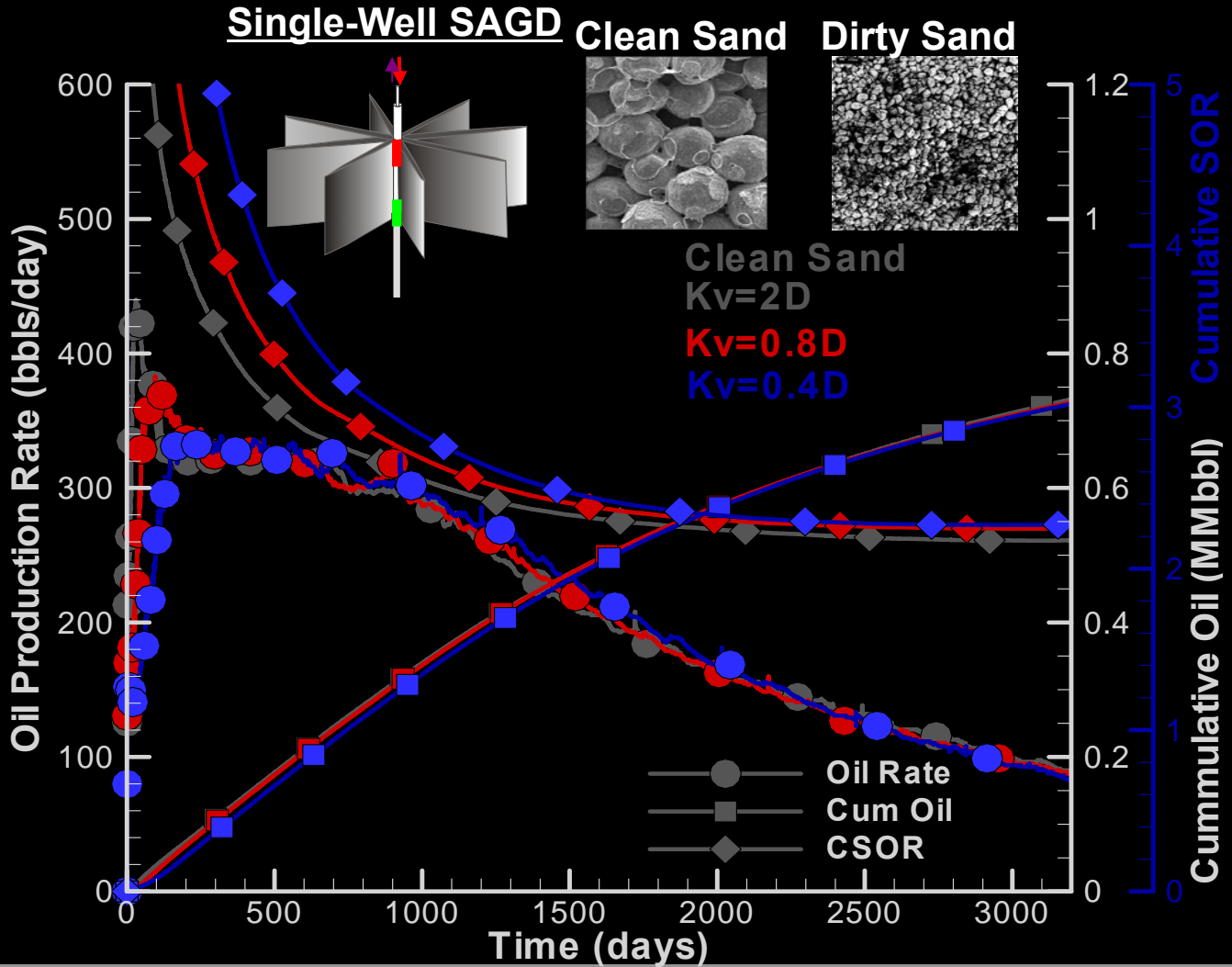
- no startup
- invariant of geology



Single-Well SAGD Completion



Single-Well SAGD vs Vert Perm



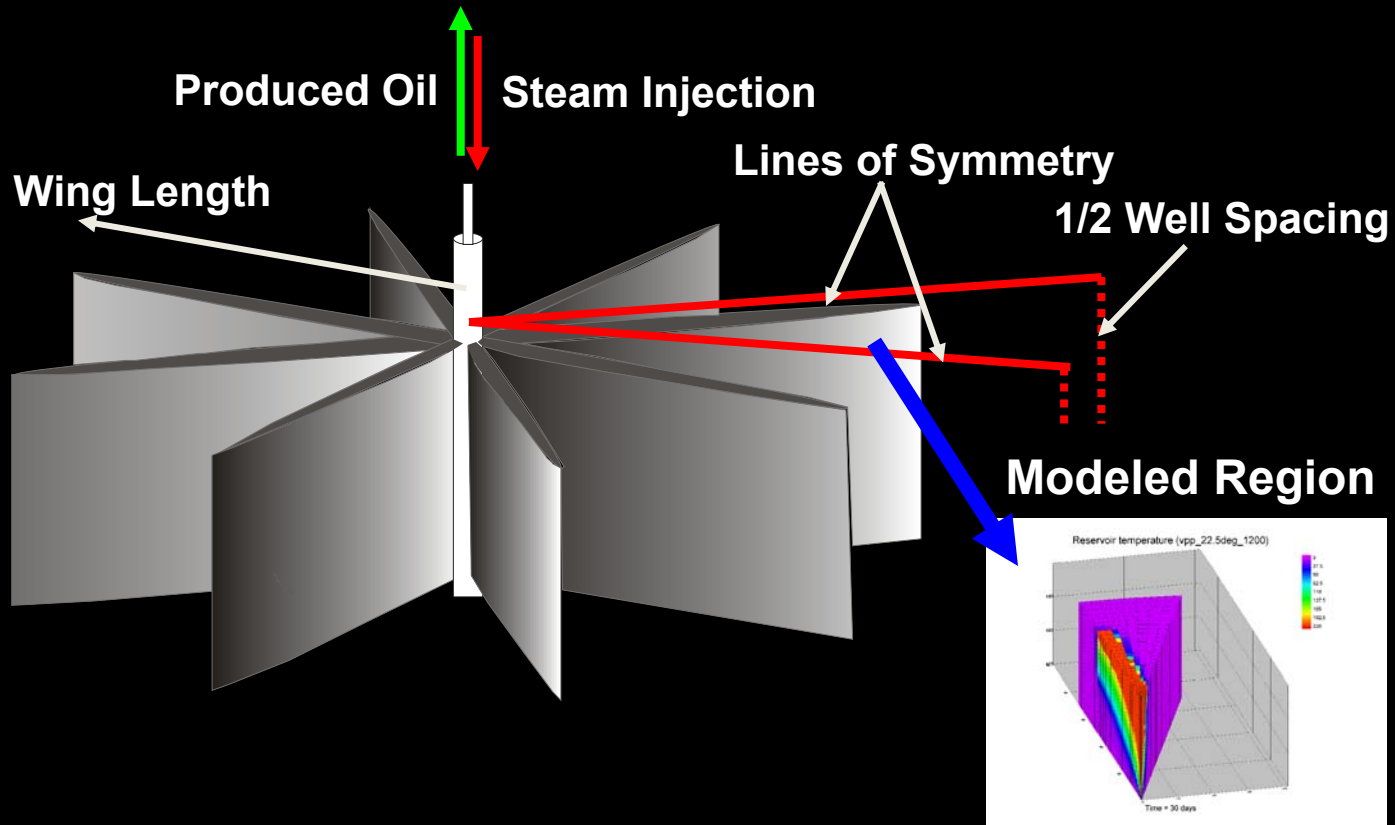
SAGD

$$q \propto \sqrt{k_v}$$

$$t \propto \frac{1}{\sqrt{k_v}}$$

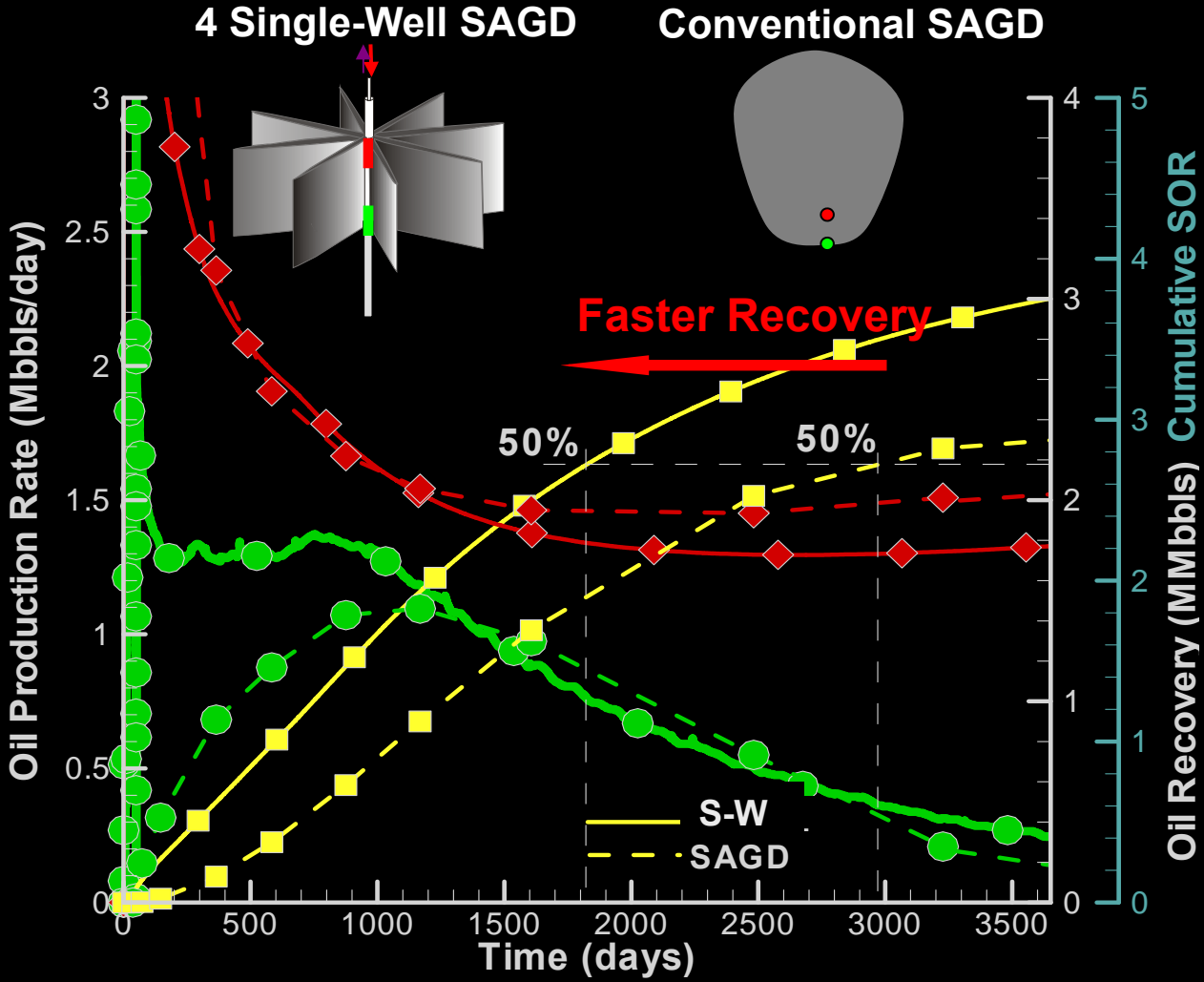
Athabasca Bitumen
Sp=1,750kPa

Reservoir Idealization



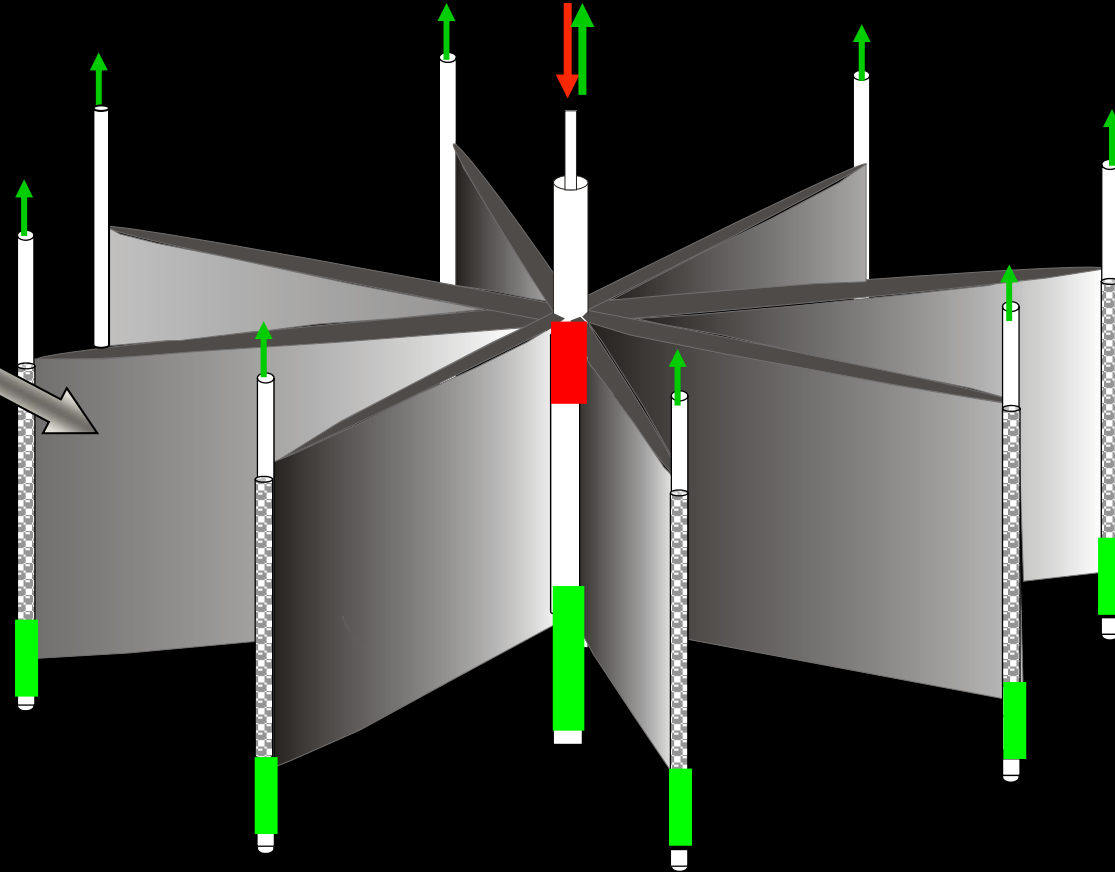
High confidence in reservoir simulations due to minimal dependence on vertical perm

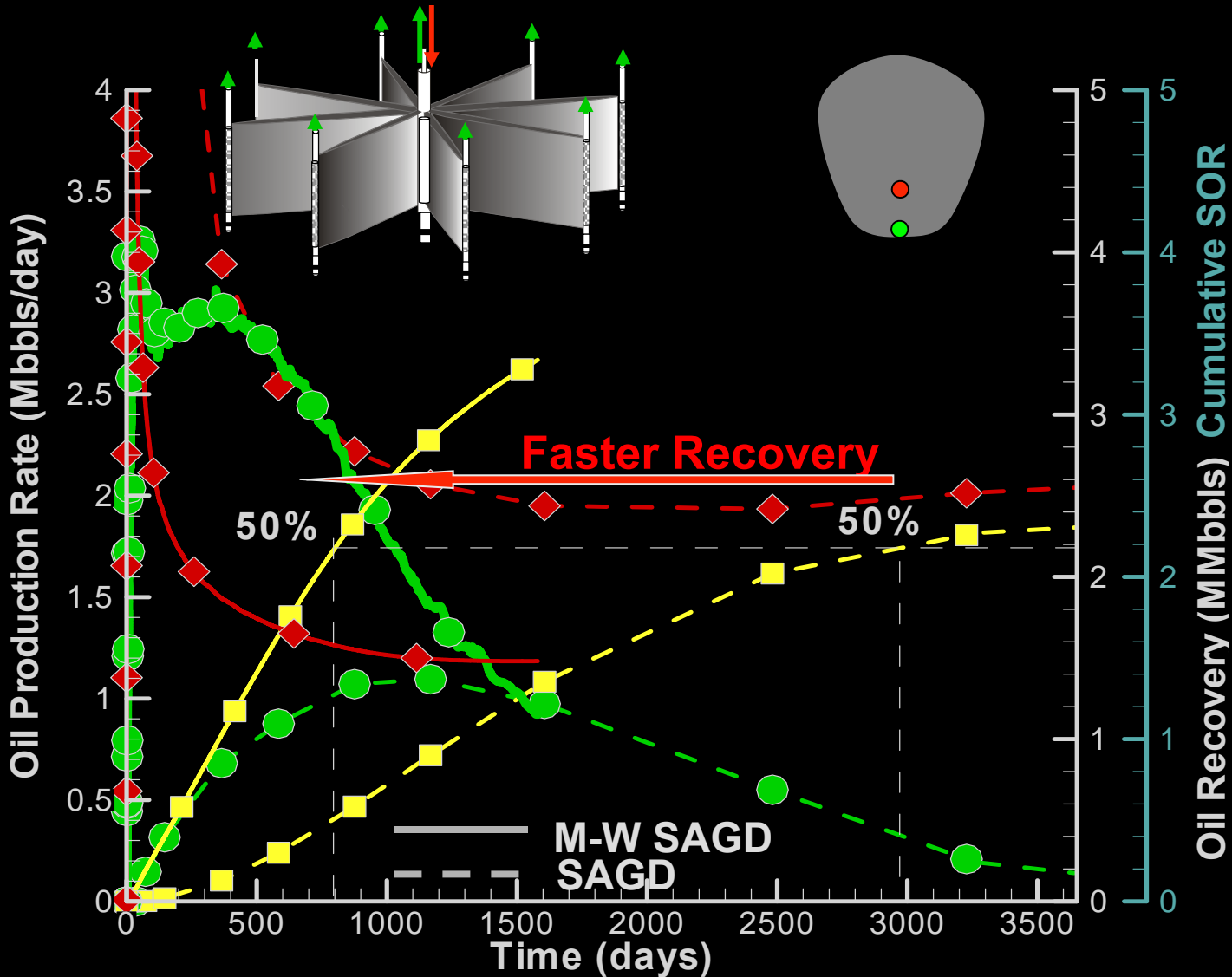
Single-Well SAGD vs Conv SAGD



Vertical Single-Well SAGD with Multiple Producers

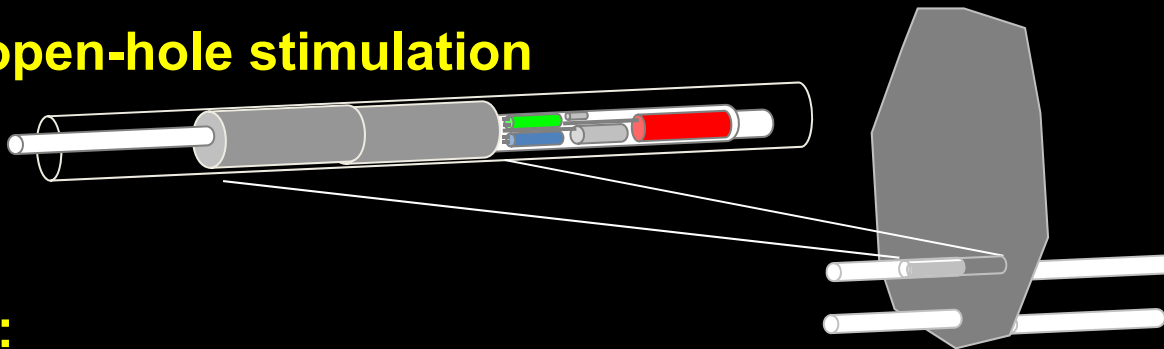
12/20 Garnet





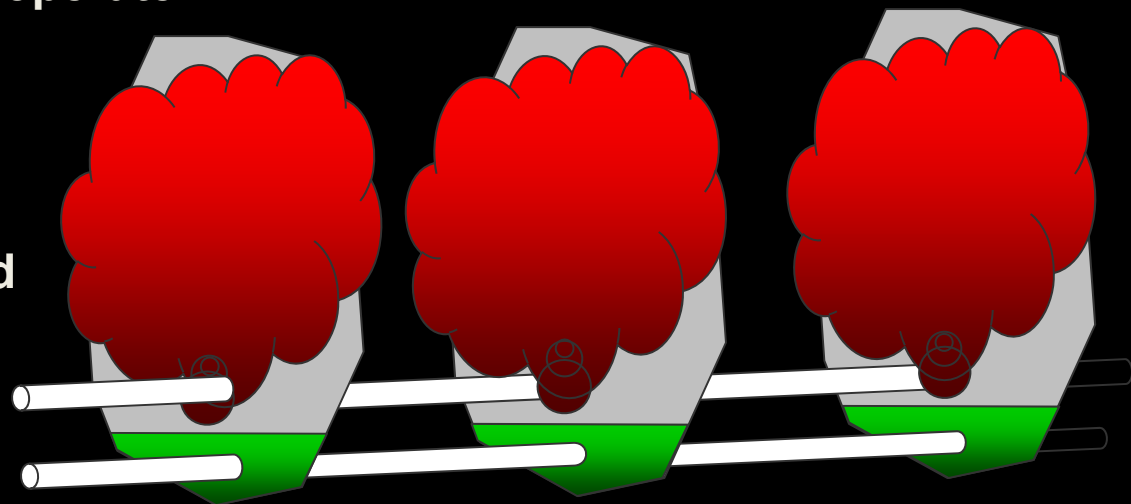
Frac Enhanced Conventional SAGD

Hz open-hole stimulation

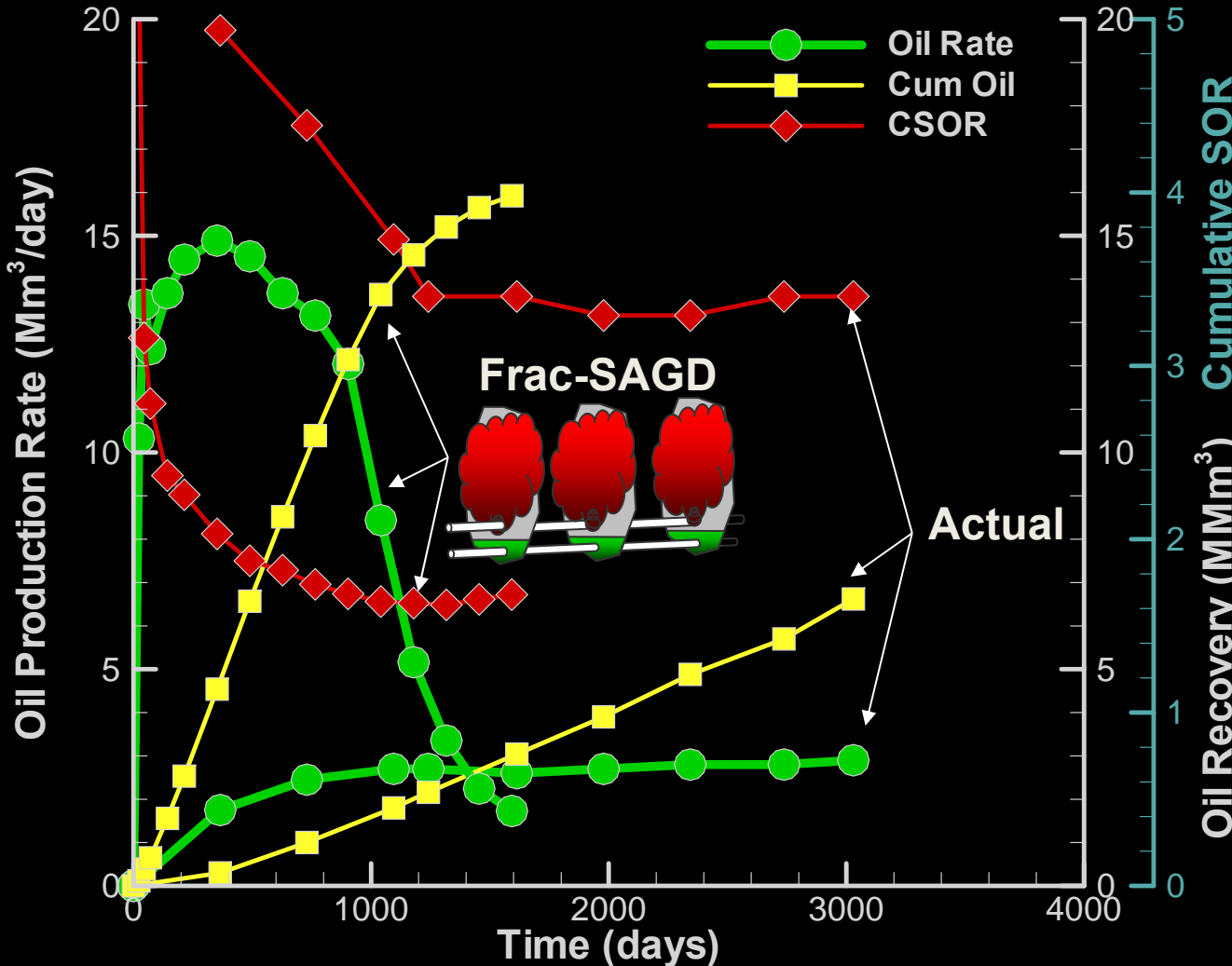


Benefits:

- Simpler & more reliable to operate
- SAGD mode at startup
- Engineer around geology
- Quick re-startup
- Operate at low pressure
- Flow conformance assured



Frac Enhanced SAGD @ Firebag



Benefits:

- Lower CSOR
- Faster Recovery
- 6x NPV₁₀

Quantified:

- Cost
\$16 vs \$32 /bbl
- Capacity
380k vs 180k bpd
- Carbon Footprint
<50% carbon/bbl
- Net Income
up by 4x Δ \$3.4B/yr*

*Bitumen \$50/bbl
52m pay, 1,850kPa, $\phi=0.3$, $S_o=0.79$

Conclusions

- **Stimulation completion dictates the outcome**
 - Mini-Frac thru' perfs or open-hole suspect in non-brittle weak formations
 - Essential to initiate frac in non-brittle formations
 - Need to re-assess earlier stimulation data & experience
- **Process not depth limited, strength limited**
- **Frac SAGD performance ~invariant of geology**
- **Frac enhance best geology first, not poorest**
 - Highest ROI, best sustainable and environmental practice
- **As built issues**
 - Permeability of planes needs to be high
 - Demonstrate azimuth control of planes from Hz wells
 - Steaming trials required to quantify performance